

Efficient Electrochemical CO₂ Conversion Powered by Renewable Energy

Douglas R. Kauffman,^{*,†} Jay Thakkar,[†] Rajan Siva,[†] Christopher Matranga,[†] Paul R. Ohodnicki,[†] Chenjie Zeng,[‡] and Rongchao Jin[‡]

[†]National Energy Technology Laboratory, United States Department of Energy, Pittsburgh, Pennsylvania 15236, United States

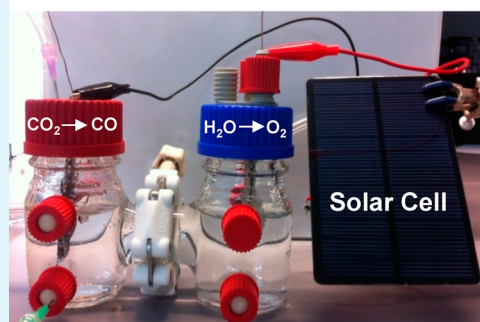
[‡]Department of Chemistry, Carnegie Mellon University, Pittsburgh, Pennsylvania 15213, United States

S Supporting Information

ABSTRACT: The catalytic conversion of CO₂ into industrially relevant chemicals is one strategy for mitigating greenhouse gas emissions. Along these lines, electrochemical CO₂ conversion technologies are attractive because they can operate with high reaction rates at ambient conditions. However, electrochemical systems require electricity, and CO₂ conversion processes must integrate with carbon-free, renewable-energy sources to be viable on larger scales. We utilize Au₂₅ nanoclusters as renewably powered CO₂ conversion electrocatalysts with CO₂ → CO reaction rates between 400 and 800 L of CO₂ per gram of catalytic metal per hour and product selectivities between 80 and 95%. These performance metrics correspond to conversion rates approaching 0.8–1.6 kg of CO₂ per gram of catalytic metal per hour. We also present data showing CO₂ conversion rates and product selectivity strongly depend on catalyst loading. Optimized systems demonstrate stable operation and reaction turnover numbers (TONs) approaching $6 \times 10^6 \text{ mol}_{\text{CO}_2} \text{ mol}_{\text{catalyst}}^{-1}$ during a multiday (36 h total hours) CO₂ electrolysis experiment containing multiple start/stop cycles. TONs between 1×10^6 and $4 \times 10^6 \text{ mol}_{\text{CO}_2} \text{ mol}_{\text{catalyst}}^{-1}$ were obtained when our system was powered by consumer-grade renewable-energy sources. Daytime photovoltaic-powered CO₂ conversion was demonstrated for 12 h and we mimicked low-light or nighttime operation for 24 h with a solar-rechargeable battery. This proof-of-principle study provides some of the initial performance data necessary for assessing the scalability and technical viability of electrochemical CO₂ conversion technologies. Specifically, we show the following: (1) all electrochemical CO₂ conversion systems will produce a net increase in CO₂ emissions if they do not integrate with renewable-energy sources, (2) catalyst loading vs activity trends can be used to tune process rates and product distributions, and (3) state-of-the-art renewable-energy technologies are sufficient to power larger-scale, tonne per day CO₂ conversion systems.

KEYWORDS: electrocatalysis, CO₂ conversion, gold nanomaterials, renewable energy, catalysis, environmental

Carbon Negative CO₂ Conversion



INTRODUCTION

Greenhouse gas mitigation is one of today's most important scientific challenges. One promising approach for addressing these emissions involves catalytically converting waste CO₂ into industrially relevant chemicals.^{1–14} This approach would reduce the carbon footprint associated with fossil fuels, provide new feedstocks for petrochemical production, and generate revenue to offset CO₂ capture and storage costs. Ultimately, CO₂ conversion can help establish a closed-loop, carbon neutral energy economy where CO₂ emissions are captured and converted into fuels and other useful products.^{1,2,9,15,16}

Electrochemical CO₂ conversion is a promising candidate for large-scale carbon management applications because it can operate with high reaction rates and good efficiency at ambient conditions.^{5,7,8,10,13,14,17–19} A typical electrochemical system contains two electrically biased electrodes: CO₂ and protons are converted into products at the negatively charged cathode, and H₂O is oxidized into O₂ and protons at the positively charged anode. CO₂ can be converted into a variety of

products,^{5,18} and Table 1 summarizes the formal potentials (E^0) and number of protons and electrons associated with several common CO₂ reduction reaction (CO₂RR) products.⁵ The total cell voltage required for CO₂RR includes potentials for both anodic and cathodic processes ($E_{\text{cell}} = E_{\text{anode}} - E_{\text{cathode}}$).¹⁰ However, cell voltages often exceed the reaction formal potentials because real-world CO₂RR and oxygen evolution reaction (OER) catalysts require overpotentials of several hundred millivolts to achieve satisfactory reaction rates. At a process level these overpotentials represent wasted energy that can lead to inefficiencies including broad product distributions at the cathode, competitive H₂ evolution from proton reduction, and reduced Faradaic efficiencies (FE; Supporting Information eq S1).^{2–7,19}

Received: May 20, 2015

Accepted: June 29, 2015

Published: June 29, 2015

Table 1. Formal Potentials (E^0) Associated with the Electrochemical CO_2 Reduction Reaction (CO_2RR) and Oxygen Evolution Reaction (OER)^{5,a}

electrode	reaction	E^0
cathode	$\text{CO}_2 + 2\text{H}^+ + 2\text{e}^- \rightarrow \text{CO} + \text{H}_2\text{O}$	-0.106
	$\text{CO}_2 + 2\text{H}^+ + 2\text{e}^- \rightarrow \text{HCOOH}$	-0.250
	$\text{CO}_2 + 4\text{H}^+ + 4\text{e}^- \rightarrow \text{HCOH} + \text{H}_2\text{O}$	-0.070
	$\text{CO}_2 + 6\text{H}^+ + 6\text{e}^- \rightarrow \text{CH}_3\text{OH} + \text{H}_2\text{O}$	0.016
	$\text{CO}_2 + 8\text{H}^+ + 8\text{e}^- \rightarrow \text{CH}_4 + 2\text{H}_2\text{O}$	0.169
	$\text{CO}_2 + 8\text{H}^+ + 12\text{e}^- \rightarrow \text{C}_2\text{H}_4 + 2\text{H}_2\text{O}$	0.064
	$2\text{H}^+ + 2\text{e}^- \rightarrow \text{H}_2$	0.000
anode	$2\text{H}_2\text{O} - 4\text{e}^- \rightarrow \text{O}_2 + 4\text{H}^+$	1.230

^a All potentials are referenced against the reversible hydrogen electrode (RHE).

Carbon balance is an important consideration for electrochemical technologies because they require electricity to promote the CO_2RR . A simple analysis shows that carbon-free energy sources must be used in CO_2RR processes to produce a net reduction in CO_2 levels. Figure 1 presents the

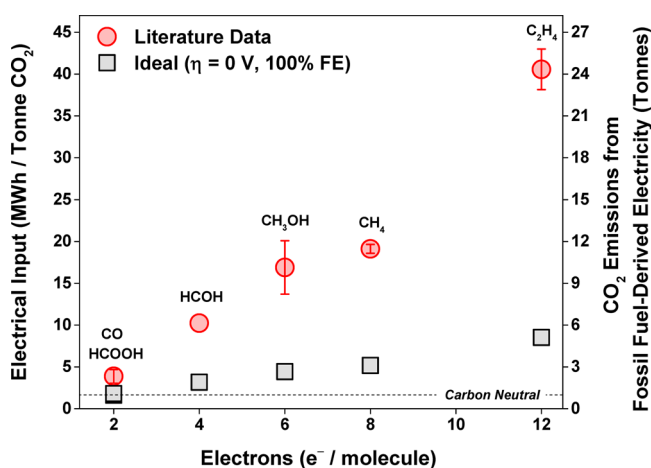


Figure 1. Electrical input required to convert 1 metric tonne of CO_2 into various products (left axis) compared with the CO_2 produced from that amount of fossil-fuel-derived electricity (right axis; $0.6 \text{ kg}_{\text{CO}_2}/\text{kWh}_{\text{electricity}}$).²⁰ Gray squares represent ideal CO_2 conversion at zero overpotential and 100% Faradaic efficiency. Red circles were calculated from literature examples of CO_2RR catalyst systems using the reported cathode voltage and FE and assuming 500 mV overpotential for OER (Supporting Information eqs S1–S4 and Tables S1 and S2).^{2,5,6,13,14,18,21–33} These data identify that fossil-fuel-derived electricity is an impractical input for CO_2 conversion systems because it produces a net increase in CO_2 emissions; i.e., the processes are *carbon positive*.

electrical input required to convert 1 metric tonne of CO_2 into various products (left axis) compared with the CO_2 produced from that amount of fossil-fuel-derived electricity (right axis). These calculations assume production rates of $0.6 \text{ kg}_{\text{CO}_2}/\text{kWh}$ for fossil-fuel-derived electricity,²⁰ and the details for developing Figure 1 are contained in eqs S2–S5 and Tables S1 and S2 of the Supporting Information. The gray squares represent ideal CO_2RR and OER with zero overpotential and 100% FE. CO_2RR energy requirements scale linearly with the number of electrons involved in the reaction, and all fossil-fuel-powered reactions, except CO and HCOOH formation, produce more CO_2 than they consume.

Real catalyst systems require substantial CO_2RR and OER overpotentials and they typically operate at less than 100% FE. To account for this nonideality Figure 1 also presents electrochemical reaction data from selected catalyst systems in the literature.^{2,5,6,13,14,18,21–33} We plotted these data using reported cathode voltages and FEs and we assumed a 500 mV overpotential for the OER (Supporting Information Table S2).² If a report listed multiple CO_2RR potentials, we chose conditions that maximized the reaction rate and FE. The overpotentials and FEs associated with real catalyst systems increase CO_2RR energy requirements so that all fossil-fuel-powered systems produce more CO_2 than they consume; i.e., they are carbon positive. Figure 1 illustrates that viable electrochemical CO_2 conversion technologies must integrate with carbon-free energy; however, very few reports have characterized renewably powered CO_2 conversion processes, the catalysts that can be utilized, or how these processes can be interfaced with carbon-friendly energy sources.^{34–37}

This work describes the development and characterization of a renewably powered electrocatalytic CO_2 conversion system. We utilize ligand-protected $\text{Au}_{25}(\text{SC}_2\text{H}_4\text{Ph})_{18}$ nanoclusters (abbreviated Au_{25}) as an extremely active and selective CO_2RR catalyst.^{13,14} Previous work from our group has demonstrated that Au_{25} promotes the electrocatalytic conversion of CO_2 into CO with 98–99+% selectivity and FE in small, 15 mL batch reactors.^{13,14} Real-world systems will require much larger, continuous flow reactors, and our current efforts focus on straightforward techniques for fabricating Au_{25} -containing electrodes and incorporating them into a simple, continuous flow system. High reaction rates, tunable product selectivity, and turnover numbers (TONs) between 1×10^6 and $4 \times 10^6 \text{ mol}_{\text{CO}_2} \text{ mol}_{\text{catalyst}}^{-1}$ were obtained with inexpensive (\$10–20 USD), consumer-grade renewable-energy sources. In this regard, we are able to demonstrate a *carbon negative* CO_2 management technology because CO_2 is converted into CO without producing additional emissions from fossil-fuel-derived electricity. These results provide a proof-of-principle demonstration of a renewably powered CO_2 conversion process and some initial performance data needed to assess the scalability of this approach. Impressive catalyst performance with off-the-shelf, renewable-energy technology illustrates that current, state-of-the-art photovoltaic and battery technologies will be sufficient for larger CO_2 conversion applications.

RESULTS AND DISCUSSION

Optimizing Catalyst Loading and $\text{CO}:\text{H}_2$ Ratios. Our group¹³ and others^{33,38} have identified relationships between nanocatalyst loading and CO_2RR activity that must be characterized for developing CO_2 conversion processes. We also illustrate later that catalyst loading and dispersion can be exploited to tune $\text{CO}:\text{H}_2$ ratios in the product stream. Catalyst dispersion is an important parameter in heterogeneously catalyzed reactions, and well dispersed particles generally show higher surface area and better reactivity compared with poorly dispersed (aggregated) particles.³⁹ Several groups have extended this concept to electrochemical reactions,^{40–45} and catalyst loading vs activity trends should be characterized to balance catalyst utilization and overall process rates.

We analyzed loading-dependent CO_2RR activity by depositing exact amounts of Au_{25} onto electrodes, and catalyst loadings are reported as the mass of Au *per* geometric electrode area ($\mu\text{g}_{\text{Au}} \text{ cm}_{\text{geo}}^{-2}$). Specific experimental details are contained in

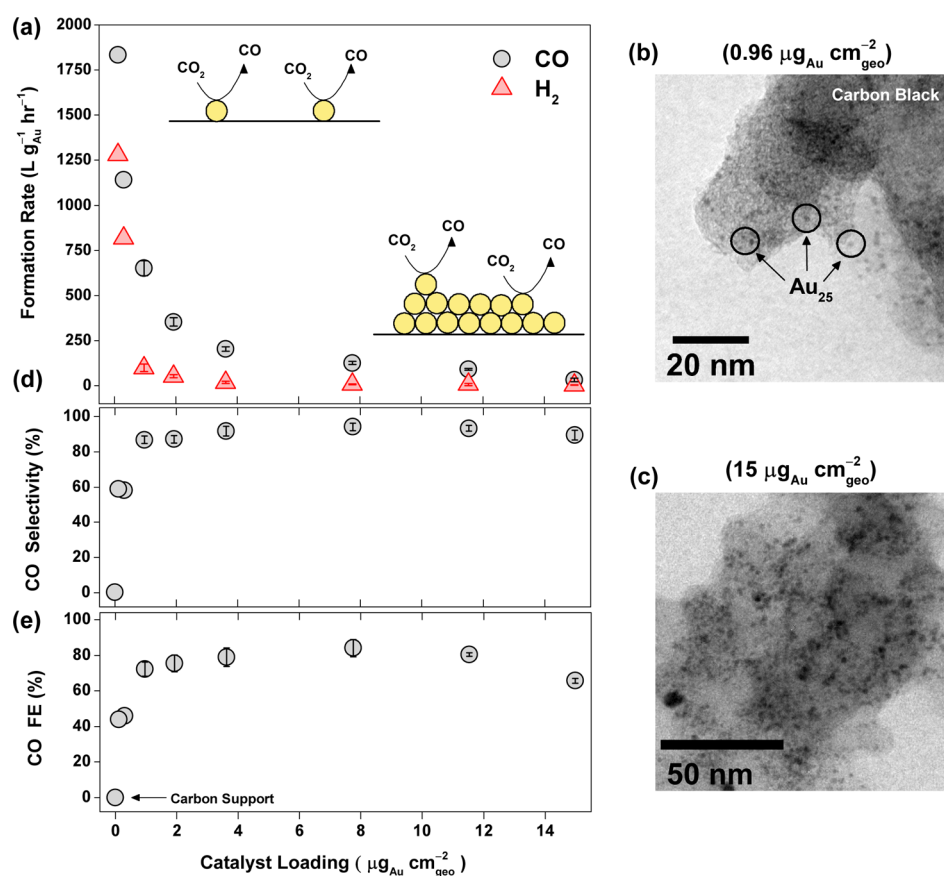


Figure 2. (a) Catalyst loading vs CO production rate for Au₂₅ operated at -1 V vs RHE and a CO₂ flow rate of 20 mL min⁻¹. The inset of panel a contains a schematic describing reactant access to well dispersed and poorly dispersed catalyst particles. (b, c) TEM images of carbon-supported Au₂₅ particles at low and high loadings. Isolated 1.4 ± 0.4 nm Au₂₅ particles were observed on the carbon black support at low loadings. Both isolated Au₂₅ particles and larger particle aggregates were observed at the higher catalyst loading. (d, e) CO selectivity and Faradaic efficiency (FE) as a function of catalyst loading. The carbon support evolved H₂ with $>99\%$ selectivity at -1 V vs RHE (Supporting Information Figure S2), and larger support-to-catalyst ratios in the low-loading regime decreased the CO selectivity and FE for Au₂₅ catalysts. Error bars represent the standard deviation from three 1 h electrolysis runs.

the Supporting Information. Briefly, CO₂ was bubbled into the cathode compartment electrolyte (catholyte) at specific flow rates (mL min⁻¹) and a constant potential was applied to the Au₂₅-containing cathode with a potentiostat. The effluent gas stream was collected and the reaction products were analyzed every 30 min with gas chromatography. We report the product formation rates as liters of gas produced *per gram Au per hour* (L g_{Au}⁻¹ h⁻¹), and FE values were calculated from the integrated electrolysis charge and the detected reaction products (Supporting Information eq S1).

Figure 2 summarizes the relationship between CO₂RR rate, product selectivity, FE, and catalyst loading at an applied potential of -1 V vs RHE and a CO₂ flow rate of 20 mL min⁻¹. Figure 2a shows higher CO formation rates are associated with lower catalyst loadings. In fact, we observed an approximate 130-fold increase in mass-normalized CO production rates when the catalyst loading was reduced from 15 to 0.1 μg_{Au} cm_{geo}⁻². The inset of Figure 2a describes our proposed mechanism for loading-dependent CO₂RR rates. Low catalyst loadings produce well dispersed, spatially separated Au₂₅ catalysts that do not compete for incoming reactants.^{40–45} This scenario produces high CO₂RR rates because reactants can easily access the Au₂₅ surface and each particle can function as an isolated reaction center. Conversely, high catalyst loadings produce closely spaced particles and/or larger particle

aggregates. These particles must compete for incoming reactant molecules, and the system shows lower mass-normalized CO₂RR rates. Transmission electron microscopy (TEM) supports this hypothesis, and we find well dispersed particles at lower catalyst loadings and aggregated particles at higher loadings (Figure 2b,c and Supporting Information Figure S1). The 1–2 nm size of apparently isolated Au₂₅ particles is consistent with the expected particle size,^{46–48} and previous work has shown the larger structures on high-loading electrodes represent closely spaced and/or aggregated Au₂₅ particles, rather than larger Au nanocrystals.¹³ We also observed increased H₂ evolution at low catalyst loadings (Figure 2d,e). The carbon electrode and carbon support evolve H₂ with $>99\%$ selectivity at -1 V vs RHE (Supporting Information Figure S2), and increased H₂ evolution occurs at low catalyst loadings because larger fractions of the carbon electrode and carbon support are exposed to solution.

We also point out that other parameters can adjust CO:H₂ ratios, reaction rates, and efficiencies. The electrode potential can also modify CO:H₂ ratios, and H₂ evolution becomes dominant at potentials more negative than -1.4 V (Supporting Information Figure S3). Finally, the rate at which CO₂ flows into the catholyte also influences catalytic activity, and higher CO₂ flow rates produced larger reaction rates, FEs, and product selectivity (Supporting Information Figure S4); however, this

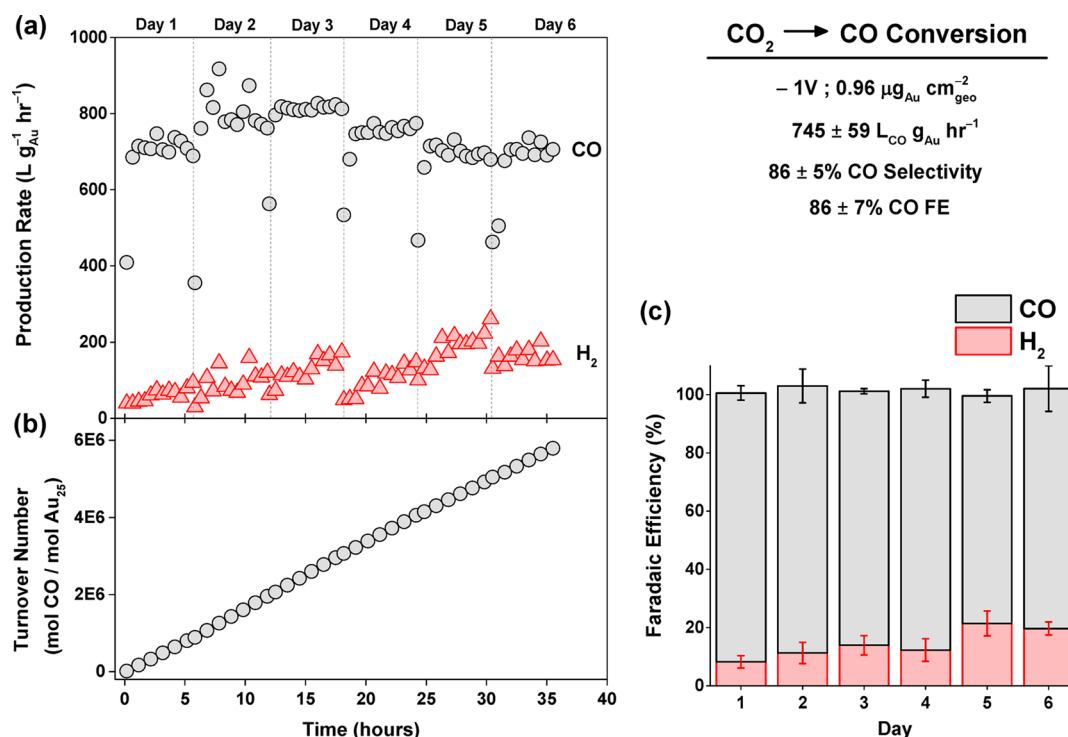


Figure 3. Day-to-day (a) product formation rates, (b) cumulative turnover number (TON, mol of CO/(mol of Au₂₅)), and (c) Faradaic efficiency during a 36 h CO₂RR experiment. The electrode contained 0.96 μg_{Au} cm_{geo}^{–2}, it was operated at –1 V vs RHE, and CO₂ was bubbled into solution with a flow rate of 50 mL min^{–1}. Daily current vs time curves are presented in Supporting Information Figure S7.

effect was small beyond flow rates larger than 50 mL_{CO₂} min^{–1}. Based on the preceding data, we chose conditions that selectively produced CO, including a catalyst loading of 0.96 μg_{Au} cm_{geo}^{–2}, a cathode voltage of –1 V vs RHE, and a CO₂ flow rate of 50 mL min^{–1}. These conditions produced CO at 810 ± 11 L g_{Au}^{–1} h^{–1} with better than 90% CO selectivity and FE during 1 h electrolysis runs. We chose conditions that favored selective CO production to characterize maximum TOF, TON, and catalyst stability, but one could target other CO:H₂ ratios by simply adjusting the catalyst loading, operating voltage, and/or CO₂ flow rate as described previously. Efficient and tunable product formation will be important for scaled-up electrochemical CO₂RR because downstream conversion of CO and H₂ into CH₄, methanol, or Fischer–Tropsch products requires different CO:H₂ ratios.²¹

Long-Term Performance. We evaluated long-term CO₂RR performance at conditions favoring selective CO formation (0.96 μg_{Au} cm_{geo}^{–2}, –1 V_{cathode}; 50 mL_{CO₂} min^{–1}), and Figure 3 presents potentiostat-controlled CO₂RR over 6 days. The electrolysis was run for 5–6 h each day to mimic realistic, on-demand usage that is known to degrade catalysts and carbon electrodes in real-world applications such as fuel cells.⁴⁹ Gas samples were collected every 30 min, but we excluded the first daily samples from data analysis because our system required ~45 min to achieve steady state operation. We found average CO formation rates of 745 ± 59 L g_{Au}^{–1} h^{–1}, CO selectivities of 86 ± 5%, and CO FEs of 86 ± 7% during the long-term CO₂RR. We determined an average turnover frequency (TOF) of 46 ± 3 mol_{CO} mol_{Au₂₅}^{–1} s^{–1}, a cumulative TON approaching 6 × 10⁶ mol_{CO} mol_{catalyst}^{–1}, and an overall FE of 102 ± 6% accounting for both CO production and H₂ evolution. Postreaction TEM and XPS analysis showed some particle coarsening and binding energy shifts in the Au 4f and

ligand S 2p spectral regions (Supporting Information Figures S5 and S6). Alivisatos and co-workers described the aggregation of ligand-free Au nanoparticles during CO₂ electrolysis,⁵⁰ and our results suggest ligand desorption allowed some particle sintering during extended electrolysis experiments. Ligand-free Au particles demonstrate lower CO selectivity,⁵¹ and a combination of ligand desorption, particle sintering, and/or H₂ evolution from the carbon support may gradually reduce CO selectivity. However, this phenomenon may not present a significant problem in systems that operate at lower voltages and/or target H₂-rich CO:H₂ product streams.

Mass activity (A g^{–1}) is another metric that quantifies electrocatalytic current with respect to catalyst mass. Au₂₅ demonstrated long-term CO₂RR mass activity of 1656 ± 163 A g_{Au}^{–1} based on the daily current (Supporting Information Figure S7), daily average CO FE (Figure 3c), and total Au loading (12.5 μg). Previous rotating disk electrode experiments produced Au₂₅ mass activities approaching 3900 A g_{Au}^{–1} at –1 V vs RHE.¹³ In the present case, slower reactant transport to the stationary planar electrodes likely reduced mass activity compared with RDE studies, and real-world systems would need to optimize the electrode geometry and solution agitation to maximize reaction rates. In comparison, Kenis and co-workers reported 2700 A g^{–1} for CO production at –0.8 V vs RHE with 1 cm^{–2} Ag/TiO₂-decorated gas diffusion electrodes,³⁸ Alivisatos and co-workers reported ~760 A g^{–1} for CH₄ production at –1.25 V vs RHE with 7 nm Cu nanoparticles,³³ we reported 20–60 A g^{–1} for CO production at –1.0 V vs RHE with sub-10 nm copper oxide nanoparticles,²⁴ and Peterson and co-workers reported 14 A g^{–1} for CO production at –0.9 V vs RHE with 4 nm Au NPs.²¹ It is unclear if poor catalyst dispersion artificially decreased the performance of non-Au₂₅ systems, and future electrocatalyst studies will need to evaluate

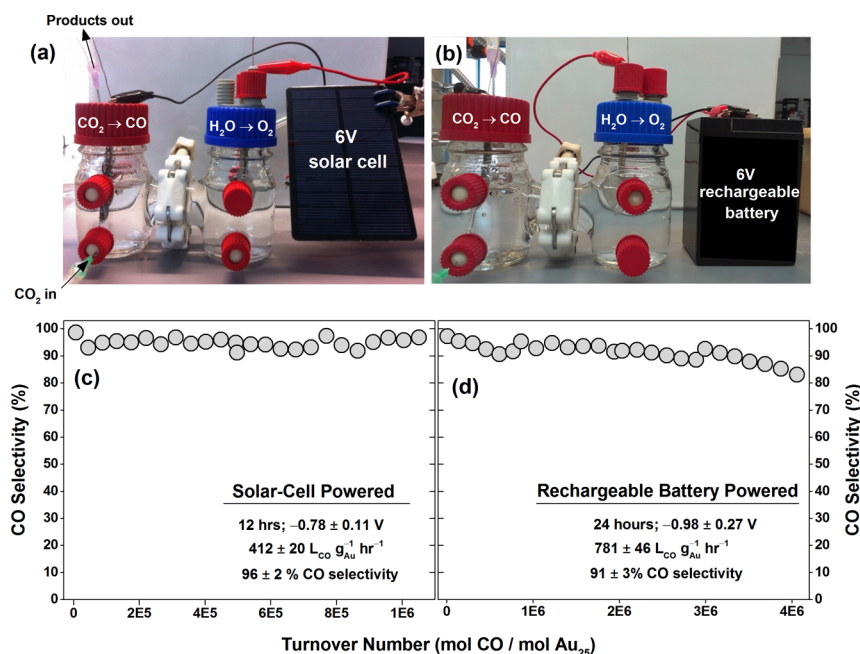


Figure 4. (a, b) Photographs of an electrochemical CO₂ reactor powered by inexpensive (\$10–20 USD) solar panels and a solar-rechargeable battery. (c, d) CO₂ → CO selectivity as a function of turnover number when powered with a solar cell or solar-rechargeable battery (where, for example, 2E5 represents 2 × 10⁵). The panels summarize operating time, average cathode voltage, CO production rate, and CO selectivity. Solar power operation mimics a 12 h sunny day, and battery-powered operation mimics nighttime hours, low-light conditions, or periods of unavailable renewable electricity. Supporting Information Figure S8 shows a photograph of the battery connected to the solar charger.

mass activity vs loading relationships when characterizing CO₂RR catalysts.

Renewable-Energy-Powered CO₂ Conversion. We have coupled our electrochemical reactor with inexpensive (\$10–20 USD), consumer-grade renewable-energy sources to mimic day and nighttime operating conditions. Panels a and b of Figure 4 present photographs of the CO₂ reactor connected to a 1.5 W, 6 V solar panel and a solar-rechargeable 6 V battery. Solar-cell-powered CO₂RR was conducted for 12 h to mimic operation during a sunny day (6 h/day, 2 days). The solar cell provided -0.78 ± 0.11 V vs RHE to the cathode and $+4.53 \pm 0.04$ V vs RHE to the Pt anode. Figure 4c summarizes the solar-powered CO₂RR operation with CO production rates of 412 ± 20 L_{CO} g_{Au}⁻¹ h⁻¹, $96 \pm 2\%$ selectivity, and a cumulative TON exceeding 1×10^6 mol_{CO} mol_{catalyst}⁻¹. Battery banks can provide stable operation in the absence of renewable energy during nighttime hours or windless conditions. A solar-rechargeable 6 V battery provided -0.98 ± 0.27 V to the cathode and $+5.49 \pm 0.27$ V to the anode (Supporting Information Figure S8). Figure 4d summarizes the battery-powered operation with a CO production rate of 781 ± 46 L_{CO} g_{Au}⁻¹ h⁻¹, $91 \pm 3\%$ selectivity, and a cumulative TON exceeding 4×10^6 mol_{CO} mol_{catalyst}⁻¹ over 24 h of operation (6 h per day, 4 days). Incorporating electronics to individually control electrode potentials could reduce the anode overpotential and tune the cathodic reaction rate and product selectivity. High catalyst performance from commonly available renewable-energy power sources provides a compelling case that current, state-of-the-art renewable-energy technologies are sufficient to power industrial CO₂RR processes and that new photovoltaic and energy storage technologies are not needed to advance this process.

Estimates for Larger-Scale CO₂ Conversion Systems. The reaction rate, FE, and energy input data presented earlier enables us to make simple estimates of the process require-

ments and expected performance on larger scales. We acknowledge that many variables can impact the performance of a particular system, including batch vs continuous flow operation, electrolyte temperature, composition, concentration and pH, gas inlet and outlet pressures, interelectrode separation, and CO₂ residence time.^{52–54} Some of these considerations are beyond the scope of this work; however, we can make performance estimates for larger-scale systems with metrics similar to our Au₂₅-based system. For example, a system with performance similar to Au₂₅ operating with a cathodic voltage of -1 V, an anodic voltage of $+1.73$ V, and 87% FE would require 3.82 MWh to convert 1 metric tonne of CO₂ into CO (Supporting Information eqs S2–S5). Energy requirements will increase for more complex products and/or less efficient catalysts, but they are accessible with state-of-the-art renewable-energy technology. For example, solar installations can produce 3.9 MWh acre⁻¹ day⁻¹ assuming a daily solar irradiance of 6 kWh m⁻² and 16% photovoltaic efficiency.² Our experimental data provide an upper CO₂ conversion capacity of 1.0 tonne of CO₂ acre⁻¹ day⁻¹ for photovoltaic-powered systems with performance similar to Au₂₅. A 1.0 MW wind turbine operating at 25% capacity could produce 6 MWh day⁻¹, and we estimate an upper CO₂ conversion capacity of 1.6 tonnes of CO₂ day⁻¹ turbine⁻¹ for wind-powered CO₂ conversion systems with performance similar to Au₂₅. Other renewable power sources such as geothermal or hydroelectric power are also suitable energy inputs, and the United States produced approximately 4.8×10^8 MWh of electricity from noncombustible renewable-energy sources in 2014.⁵⁵ Utilizing 1% of the renewable energy currently produced in the United States could convert between 2.5×10^5 and 1.2×10^6 metric tonnes of CO₂ into CO, HCOH, CH₃OH, or CH₄ using the catalysts summarized in Figure 1. Installing dedicated renewable-energy sources would increase CO₂ capacity, and excess

electricity could be fed back into the electrical grid to further reduce CO₂ emissions. These estimates show that tonne *per* day CO₂ conversion systems are feasible with current catalyst systems and renewable-energy sources.

CONCLUSIONS

Our estimates indicate that state-of-the-art renewable technologies are sufficient to power large-scale CO₂ conversion systems operating at tonne *per* day rates. We have shown that impressive catalytic reaction rates, product selectivities, and efficiencies can be achieved with off-the-shelf, consumer-grade renewable-energy sources. We expect other catalyst systems will show similarly impressive performance when coupled to renewable-energy sources, and our work highlights the potential for renewably powered electrochemical CO₂ conversion systems. The anode catalyst is another important aspect of CO₂ conversion because it consumes roughly half of the electrical input. Improving the anode efficiency and reducing OER overpotentials will decrease the overall energy requirements for CO₂ conversion and make this carbon mitigation strategy even more practical.

ASSOCIATED CONTENT

Supporting Information

Text containing experimental details, tables listing ideal energy requirements for CO₂ conversion and energy requirements for selected catalytic conversions, and figures showing SEM and TEM images, product formation rates, H₂ and CO selectivities, Faradaic efficiencies, XPS of Au 4f and S 2p regions, CO₂RR currents, and photograph of solar-rechargeable battery. The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsami.5b04393.

AUTHOR INFORMATION

Corresponding Author

*E-mail: Douglas.Kauffman@NETL.DOE.GOV.

Notes

The authors declare no competing financial interest.

ACKNOWLEDGMENTS

R.J. acknowledges research support from AFOSR. This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights.

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